



Masonry Walls and Energy Codes –Alternative Energy Code Compliant Designs for Single Wythe Masonry Structures in Hawaii

Session 3

September 2019 – Hawaii

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Introduction

- Discuss two phase investigation of energy efficient design of typical structures that use exterior masonry and concrete walls.
- Phase 1 – Looked at prescriptive approach, R , U and Com Check Trade off approaches
- Phase 2 - looked at whole building energy analysis and alternative approaches.

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Introduction

- Compliance with the increasing stringent prescriptive code provisions is becoming increasingly more difficult, and new solutions are necessary.
- The recent Hawaiian adoption of IECC 2015 complicated cost effective energy efficient design in this state by now prescriptively requiring continuous insulation for exterior masonry walls. – Residential & Non. (solid grouting)

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IECC Prescriptive R table

CLIMATE ZONE	1		2		3		4		5		6		7		8	
	All other	Group R	All other	Group R	All other	Group R	All other	Group R	All other	Group R	All other	Group R	All other	Group R	All other	Group R
Roofs																
Insulation entirely above roof deck	U-0.048	U-0.039	U-0.039	U-0.039	U-0.039	U-0.039	U-0.032	U-0.032	U-0.032	U-0.032	U-0.032	U-0.032	U-0.028	U-0.028	U-0.028	U-0.028
Metal buildings	U-0.044	U-0.035	U-0.035	U-0.035	U-0.035	U-0.035	U-0.030	U-0.030	U-0.030	U-0.030	U-0.030	U-0.030	U-0.029	U-0.029	U-0.029	U-0.029
Attic and other	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.027	U-0.021	U-0.021	U-0.021	U-0.021
Walls, above grade																
Mass	U-0.151	U-0.151	U-0.151	U-0.123	U-0.123	U-0.104	U-0.104	U-0.090	U-0.090	U-0.090	U-0.080	U-0.071	U-0.071	U-0.061	U-0.061	U-0.061
Metal building	U-0.079	U-0.079	U-0.079	U-0.079	U-0.079	U-0.052	U-0.052	U-0.052								
Metal framed	U-0.077	U-0.077	U-0.077	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.057	U-0.057	U-0.052	U-0.045
Wood framed and other	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.064	U-0.051	U-0.051	U-0.051	U-0.036	U-0.036
Walls, below grade																
Below-grade wall ^a	C-1.140 ^b	C-0.119	C-0.119	C-0.119	C-0.119	C-0.119	C-0.119	C-0.119	C-0.092	C-0.092	C-0.092	C-0.092				
Floors																
Mass ^c	U-0.322 ^d	U-0.322 ^d	U-0.107	U-0.087	U-0.076	U-0.076	U-0.076	U-0.076	U-0.076	U-0.076	U-0.074	U-0.064	U-0.054	U-0.054	U-0.055	U-0.055
Joist/framing	U-0.066 ^e	U-0.066 ^e	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033	U-0.033
Slab-on-grade floors																
Unheated slabs ^f	F-0.73 ^g	F-0.54	F-0.54	F-0.54	F-0.54	F-0.54	F-0.54	F-0.52	F-0.40	F-0.40	F-0.40	F-0.40				
Heated slabs ^f	F-0.70	F-0.70	F-0.70	F-0.70	F-0.70	F-0.70	F-0.65	F-0.65	F-0.65	F-0.65	F-0.65	F-0.58	F-0.55	F-0.55	F-0.55	F-0.55
Opaque doors																
Swinging	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.61	U-0.37	U-0.37	U-0.37	U-0.37	U-0.37

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International Energy Conservation Code

IECC Section C 402 - prescriptive R requirements for building envelopes.

Zone 1 minimum thermal resistance (R) values - mass walls above grade (typical masonry walls) - minimum continuous insulation R= 5.7 °F. ft².hr/BTU. IECC Section C402.2.3 indicates that any integral insulation of CMU block cannot be used to meet this continuous R requirement.

Footnote c in this table indicates that partially grouted (32" O.C.) ASTM C 90 block walls do not need continuous insulation if the ungrouted cells of the block are filled with materials having a maximum thermal conductivity of 0.44 Btu-in/h-f² °F.

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ASHRE 90.1 Prescriptive R table

Table 5.5-1 Building Envelope Requirements for Climate Zone 1 (A,B,C)*

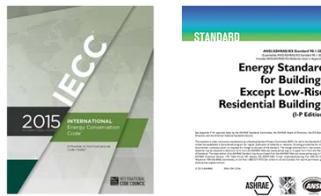
Opaque Elements	Nonresidential		Residential		Semiheated	
	Assembly Maximum	Insulation Min. R-Value	Assembly Maximum	Insulation Min. R-Value	Assembly Maximum	Insulation Min. R-Value
<i>Roofs</i>						
Insulation Entirely above Deck	U-0.048	R-20 c.i.	U-0.039	R-25 c.i.	U-0.218	R-3.8 c.i.
Metal Building*	U-0.041	R-10 + R-19 FC	U-0.041	R-10 + R-19 FC	U-0.115	R-10
Attic and Other	U-0.027	R-38	U-0.027	R-38	U-0.081	R-13
<i>Walls, above Grade</i>						
Mass	U-0.580	NR	U-0.151 ^b	R-5.7 c.i. ^b	U-0.580	NR
Metal Building	U-0.094	R-0 + R-9.8 c.i.	U-0.094	R-0 + R-9.8 c.i.	U-0.352	NR
Steel Framed	U-0.124	R-13	U-0.124	R-13	U-0.352	NR
Wood Framed and Other	U-0.089	R-13	U-0.089	R-13	U-0.292	NR
<i>Wall, below Grade</i>						
Below Grade Wall	C-1.140	NR	C-1.140	NR	C-1.140	NR
<i>Floors</i>						
Mass	U-0.322	NR	U-0.322	NR	U-0.322	NR
Steel Joist	U-0.350	NR	U-0.350	NR	U-0.350	NR
Wood Framed and Other	U-0.282	NR	U-0.282	NR	U-0.282	NR

For Climate Zone 1 shows that mass walls above grade (CMU walls) do not require insulation when used in nonresidential construction.

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International Energy Conservation Code

IECC Allows use of ASHRE 90.1 Instead of IECC

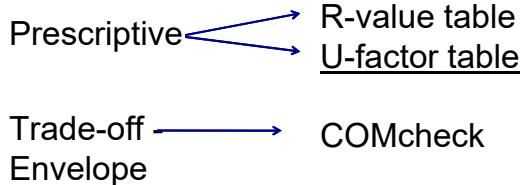


"C401.2 Application. Commercial buildings shall comply with one of the following:

1. The requirements of ANSI/ASHRAE/IESNA 90.1.
2. The requirements of Sections C402 through C405. In addition, commercial buildings shall comply with Section C406 and tenant spaces shall comply with Section C406.1.1.
3. The requirements of Sections C402.5, C403.2, C404, C405.2, C405.3, C405.4, C405.6 and C407. The building energy cost shall be equal to or less than 85 percent of the standard reference design building."

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Energy Code Compliance – IECC – Hawaii – Phase 1

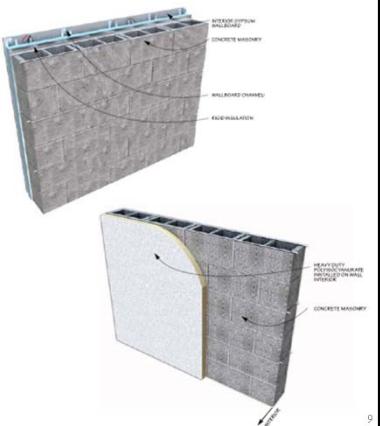


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Prescriptive R-Value Compliance

Continuous interior insulation:

- R 5.7 – Use 1.5 inches of Expanded Polystyrene - stucco ext. With finishes as shown - Solid grouting
- Using U-factor – 0.151
Can reduce $\frac{3}{4}$ " of insulation.

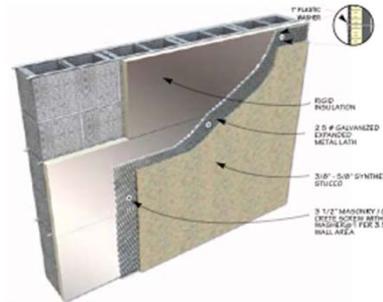


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Prescriptive R-Value Compliance - Hawaii

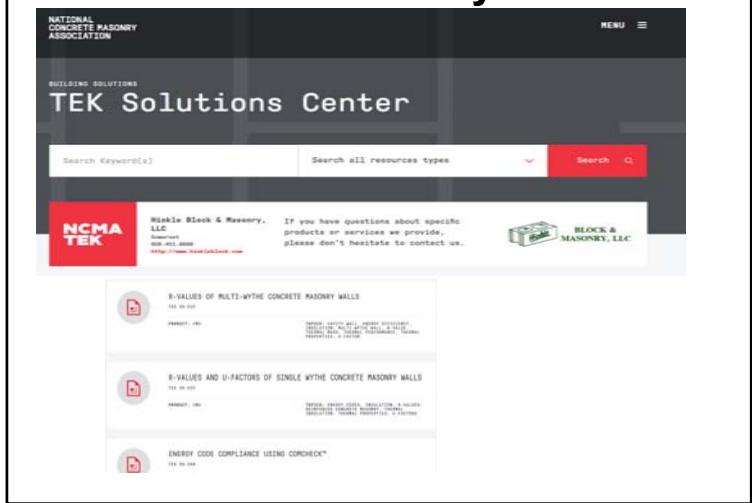
Continuous exterior insulation:

- R 5.7 – Use 1.5 inches of Expanded Polystyrene - stucco ext. – Solid grouting
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-



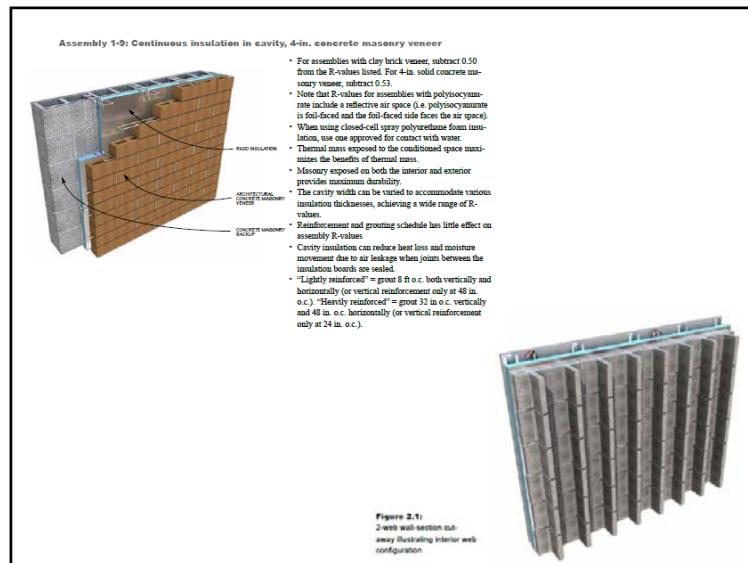
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Where Do I Find Masonry U-Factors?



Many wall configurations addressed in Catalogue





**SINGLE WYTHE CONCRETE MASONRY ASSEMBLIES
CELL INSULATION**

Assembly 2-1: Polyurethane foamed-in-place insulation in ungrouted cells, exposed masonry (interior and exterior)

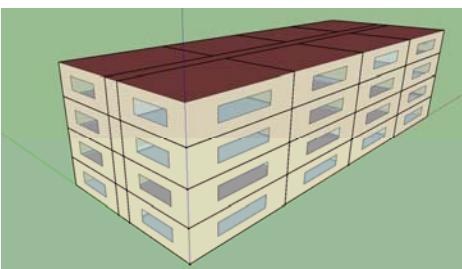
Concrete Masonry Assembly R-Values (hr·ft²·°F/Btu) and U-Factors (Btu/hr·ft²·°F)

Density of CMU, PCF	6-in. Concrete Masonry				8-in. Concrete Masonry			
	Ungrouted	Lightly Reinforced	Heavily Reinforced	Fully Grouted	Ungrouted	Lightly Reinforced	Heavily Reinforced	Fully Grouted
65	9.48 (0.105)	5.45 (0.183)	3.64 (0.275)	1.77 (0.564)	12.97 (0.077)	6.84 (0.146)	4.40 (0.227)	2.07 (0.483)
95	8.37 (0.119)	5.01 (0.200)	3.40 (0.294)	1.69 (0.592)	11.41 (0.088)	6.28 (0.159)	4.10 (0.244)	1.96 (0.509)
105	7.36 (0.136)	4.59 (0.218)	3.18 (0.315)	1.62 (0.619)	9.98 (0.100)	5.75 (0.174)	3.83 (0.281)	1.87 (0.535)
115	6.43 (0.155)	4.19 (0.239)	2.97 (0.337)	1.55 (0.645)	8.69 (0.115)	5.25 (0.191)	3.58 (0.279)	1.79 (0.559)
125	5.61 (0.178)	3.82 (0.262)	2.78 (0.360)	1.49 (0.670)	7.53 (0.133)	4.78 (0.209)	3.34 (0.299)	1.72 (0.583)
135	4.88 (0.205)	3.47 (0.280)	2.59 (0.386)	1.44 (0.693)	6.51 (0.154)	4.34 (0.230)	3.12 (0.321)	1.65 (0.605)

Density of CMU, PCF	10-in. Concrete Masonry				12-in. Concrete Masonry			
	Ungrouted	Lightly Reinforced	Heavily Reinforced	Fully Grouted	Ungrouted	Lightly Reinforced	Heavily Reinforced	Fully Grouted
65	17.44 (0.057)	8.20 (0.122)	5.05 (0.198)	2.23 (0.438)	21.91 (0.046)	9.44 (0.106)	5.66 (0.177)	2.50 (0.400)
95	15.32 (0.065)	7.56 (0.132)	4.74 (0.211)	2.15 (0.459)	19.22 (0.052)	8.75 (0.114)	5.33 (0.187)	2.39 (0.418)
105	13.36 (0.075)	6.96 (0.144)	4.45 (0.228)	2.06 (0.480)	16.74 (0.060)	8.09 (0.124)	5.03 (0.199)	2.39 (0.438)
115	11.59 (0.086)	6.38 (0.157)	4.17 (0.240)	2.00 (0.501)	14.50 (0.069)	7.45 (0.134)	4.74 (0.211)	2.21 (0.453)
125	10.01 (0.100)	5.84 (0.171)	3.92 (0.255)	1.92 (0.520)	12.49 (0.080)	6.84 (0.146)	4.46 (0.224)	2.13 (0.469)
135	8.61 (0.116)	5.32 (0.180)	3.67 (0.272)	1.86 (0.559)	10.71 (0.093)	6.25 (0.160)	4.20 (0.238)	2.06 (0.485)

* Assembly details page 37

Phase 1 - Evaluated 4 Prototype buildings typically using Masonry exterior Walls using COMCheck

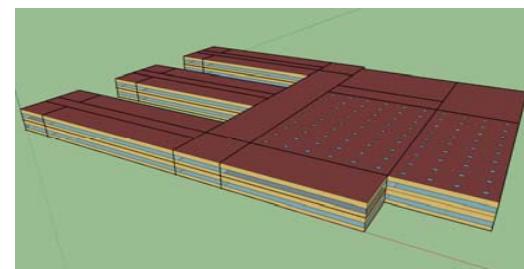


A. Midrise Apartment

The total floor area of the four story, DOE prototype midrise apartment building shown in Figure 1 is 33,741 ft² and it has an aspect ratio of 2.74. The window fraction for each orientation (north, south, east and west) is a constant 20%.

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Phase 1 - Evaluated 4 Prototype buildings typically using Masonry exterior Walls using COMCheck

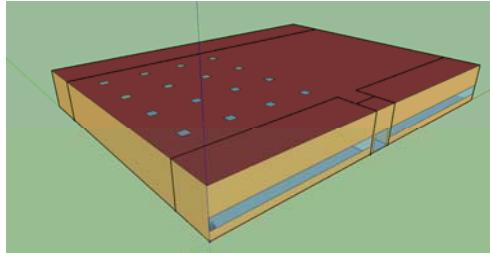


B. Secondary School

The total floor area of the two story, DOE defined secondary school building is 210,886 ft², with an aspect ratio of 1.4. The window fraction for each orientation (north, south, east and west) was a constant 33%, with ribbon windows across all facades, on both floors. Floor to floor height is 13 ft.

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**Phase 1 - Evaluated 4 Prototype buildings
typically using Masonry exterior Walls using
COMCheck**

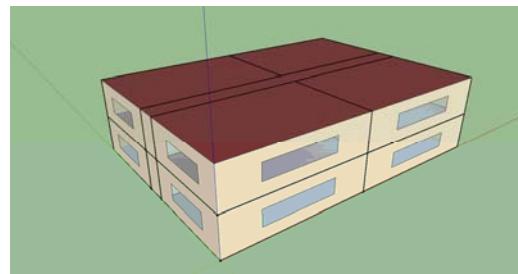


C. Stand-alone Retail

The total floor area of the one story, DOE prototype retail building is 24,692 ft², with an aspect ratio of 1.28 . The floor to ceiling height is 20 ft. The window fraction is 7.1% in total, with windows located on the street facing façade only.

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**Phase 1 - Evaluated 4 Prototype buildings
typically using Masonry exterior Walls using
COMCheck**



D . Low-rise Apartment - The total floor area of the two story, low-rise apartment building is 8,435 ft², with an aspect ratio of 1.37. This structure was based on the midrise apartment, but modified to represent a low-rise construction configuration common in Hawaii. The window fraction for each orientation (north, south, east and west) was a constant 20%.

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COMcheck

- easy way to take advantage of trade-offs, ie, increase roof insulation to reduce wall or window requirements.
- program shows if the envelope complies, and how close it is to compliance
- allows individual elements to be tweaked for compliance, revisions are quick and easy.
- **Trade offs are for envelope only**

From NCMA
Presentation

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COMcheck

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COMcheck

- The trade-off analysis clearly shows that, for the four prototype buildings investigated, no reasonable amount of roof insulation, or more thermally resistant windows could be used to make uninsulated fully grouted exterior concrete masonry or bare concrete walls code compliant through a trade-off analysis alone.

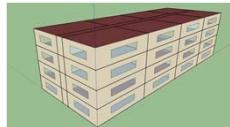
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Phase 2 Whole Building Analysis - Using 4 Prototypes

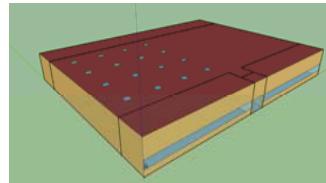
- Energy Budget method requires same yearly energy cost of prototype configured to prescriptive requirements.
- Used Openstudio and Energy plus Programs – Looked at changes in envelopes and building systems that were expected to be minimum costs.
- Also conducted a economic analysis

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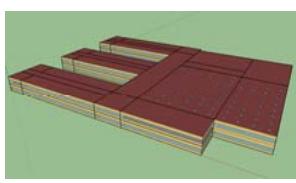
Phase 2 Whole Building Analysis



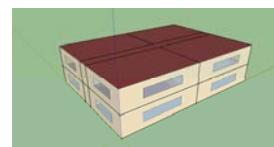
A . Mid-rise Apartment



C. Stand-alone Retail



B. Secondary School



D . Low-rise Apartment

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Baseline Configuration

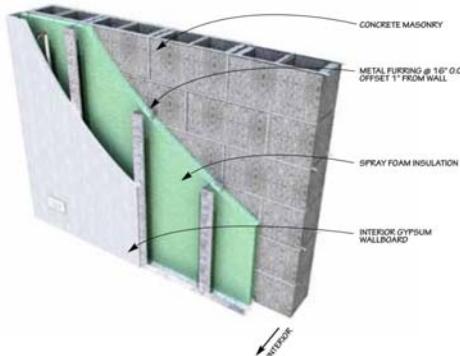


Figure 5 CMU Walls (8 in.) with Wall Insulation + 0.5 in. Gypsum Board

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Baseline Exterior Wall

Table 1 Critical Exterior Wall Assembly Configuration Properties

Type of Wall	Wall Configurations	Conductivity (Btu·in/hr·ft ² ·R)	Specific Heat (Btu/lb·R)	U factor (Btu/ft ² ·h·R)
Fully Grouted 105 pcf 8" CMU	Solid Grouted	8.400	0.209	0.528
Fully Grouted 120 pcf 8" CMU	Solid Grouted	9.600	0.211	0.566
Fully Grouted 130 pcf 8" CMU	Solid Grouted	10.7	0.220	0.591
Partially Grouted 8" CMU	Cells Insulated	3.248	0.162	0.294
Poured Concrete 120 pcf	Limestone Concrete	7.900	0.210	0.537
Poured Concrete 130 pcf	Sand and Gravel or Stone Aggregate Concrete	9.400	0.210	0.588
Poured Concrete 150 pcf	Sand and Gravel or Stone Aggregate Concrete	14.900	0.210	0.721

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Exterior Wall

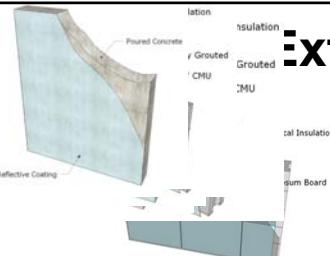


Figure 10 Exterior CMU Wall Case A

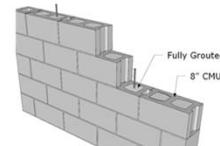


Figure 11 Exterior Wall Cases 105/120/130FM_B&D&F&G&H

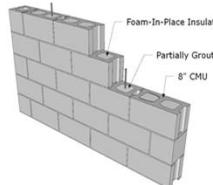


Figure 12 Exterior Wall Cases 105PM_B&D&F&G&H

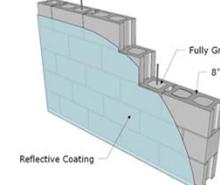


Figure 13 Exterior Wall Cases

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Exterior Wall

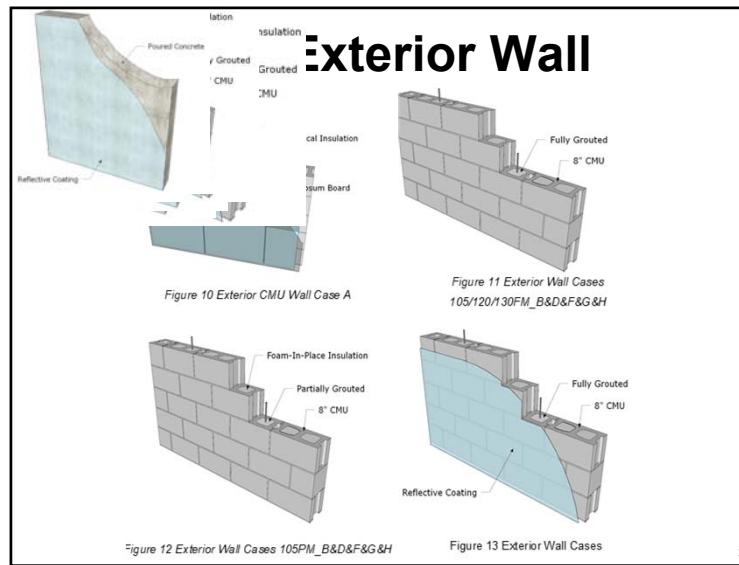


Figure 10 Exterior CMU Wall Case A



Figure 11 Exterior Wall Cases 105/120/130FM_B&D&F&G&H

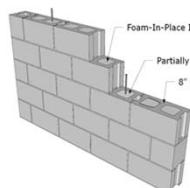


Figure 12 Exterior Wall Cases 105PM_B&D&F&G&H

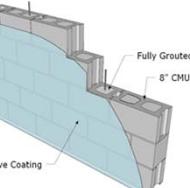


Figure 13 Exterior Wall Cases

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Baseline Exterior Wall

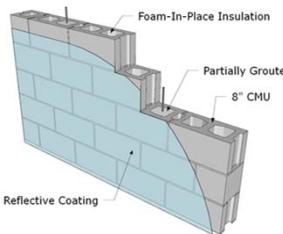


Figure 18 Exterior Wall Assumed when Calculating Target U-factor (Fully Grouted)

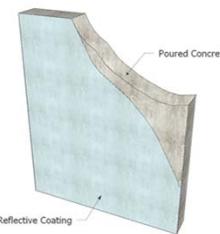


Figure 19 Exterior Wall Assumed when Calculating Target U-factor (Concrete)

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Whole Building Analysis Configurations

ALL CASE A (Include 105/120/130 pcf Fully Grouted CMU (105/120/130FM), 105 pcf Partially Grouted CMU (105PM), 120/130/150 pcf Poured Concrete (120/130/150 PC)) - The U-factor - 0.151 Btu/ft²hR). (Code minimum)

Case B

105 pcf Full Grouted CMU (105FM) CASE B -U-factor - 0.528 Btu/ft²hR.
120 pcf Full Grouted CMU (120FM) U-factor -0.566 Btu/ft²hR.
130 pcf Full Grouted CMU (130FM) - 0.591 Btu/ft²hR.
105 pcf Partially Grouted CMU (105PM) -U-factor- 0.294 Btu/ft²hR.
120 pcf Poured Concrete walls (120PC) -U-factor 0.537 Btu/ft²hR.
130 pcf Poured Concrete walls (130PC) -U-factor 0.588 Btu/ft²hR.
150 pcf Poured Concrete walls (150PC) -U-factor 0.721 Btu/ft²hR.

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Whole Building Analysis Configurations

Case C – For all “C” cases, the exterior surface reflectance of the walls was increased to 0.64. (consistent with Hawaii Energy Code amendments for exceptions for lightweight walls).

Case D - Overhangs with a Projection Factor (PF) of 0.3 are added to all fenestrations in the basic (Case B) configurations.

Case E - Combined the Overhang of Case D and the increased wall reflectance of Case B.

Case F - Approximately twice the roof insulation was applied to the basic (CASE B) configurations (Roof U-factor decreased to 0.146 W/m²K (0.026 Btu/ft²hR).

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Whole Building Analysis Configurations

Case G - Lighting is a significant part of total energy use in most buildings, the impact of more efficient lighting was investigated. Although conventional wisdom suggests that LED lighting is much more efficient than conventional systems, a recent study by the DOE (“LED Replacements for Four-Foot Linear Fluorescent Lamps)[1], suggests that some fluorescent lamps can have similar luminaire efficacy (lumens/watt) as LEDs. Therefore, in this research, we assumed that there would only be a 10% reduction in lighting energy with LED lighting.

Case H – Higher efficiency HVAC systems were investigated. In this case, the HVAC system efficiency in the basic building configuration (case B) was increased. As per Trane product catalogs, models were listed that showed an increase from the Code minimum values of about 8% (based on EERE values). Thus, the HVAC coefficient of performance (COP) was increased by 8% in the EnergyPlus models.

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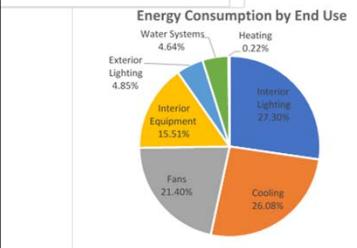
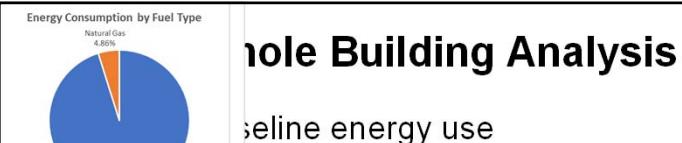
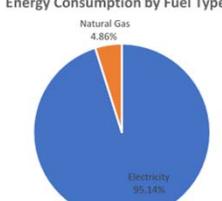
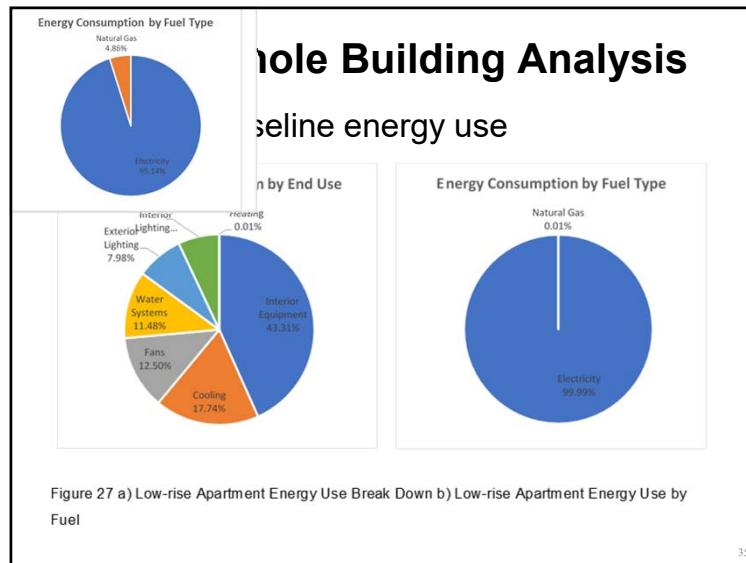
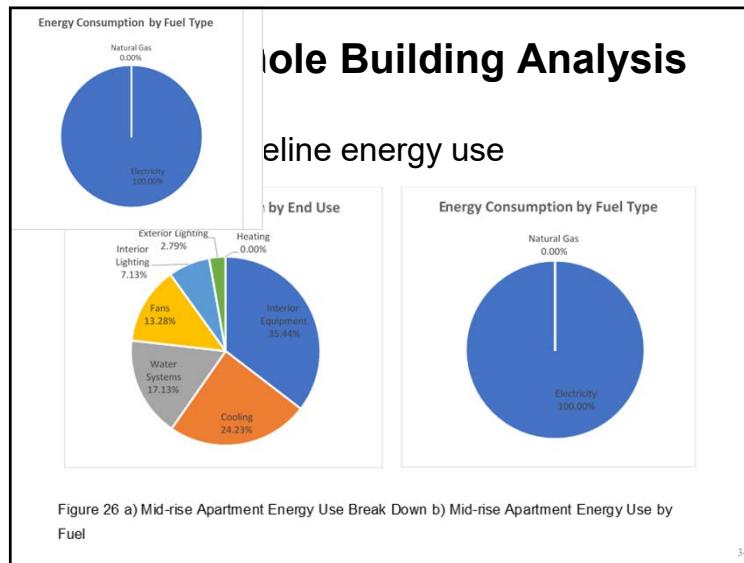
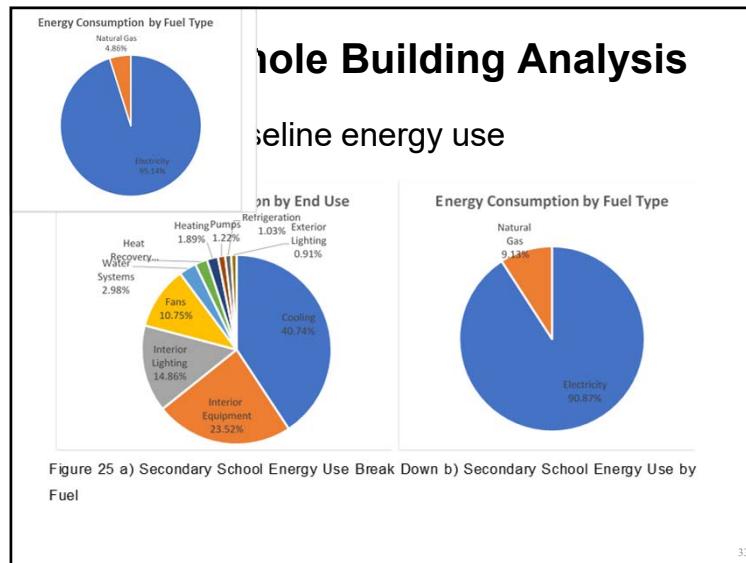
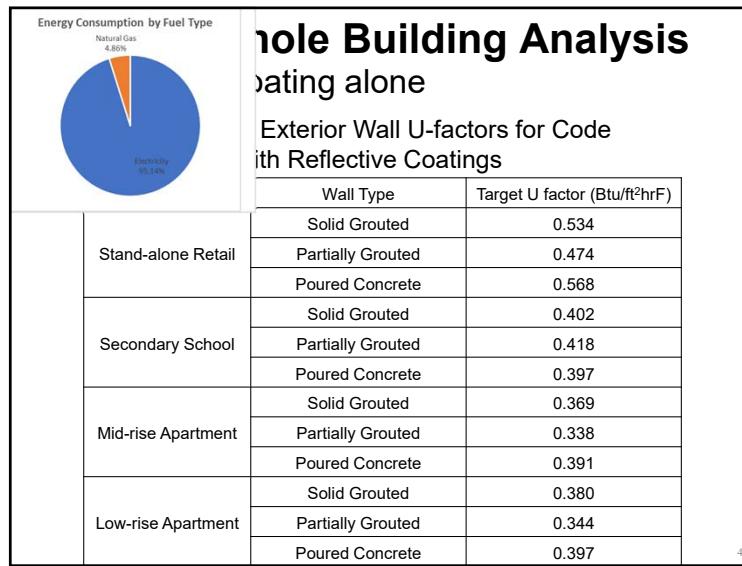
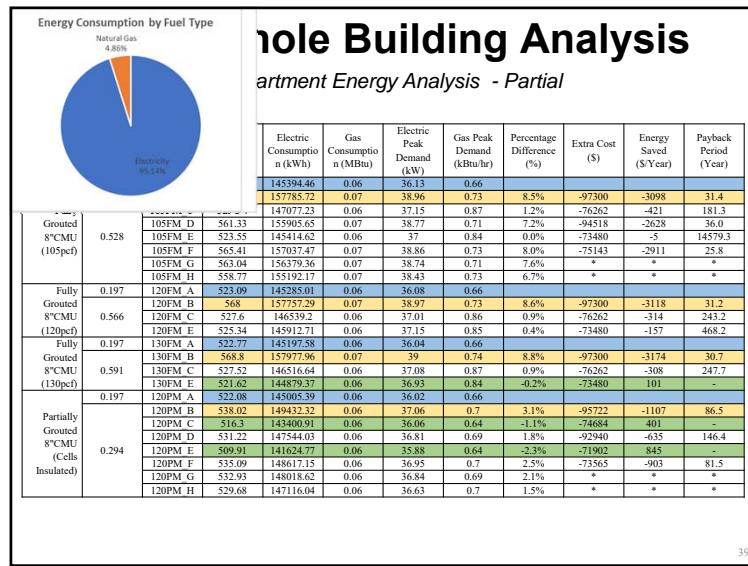
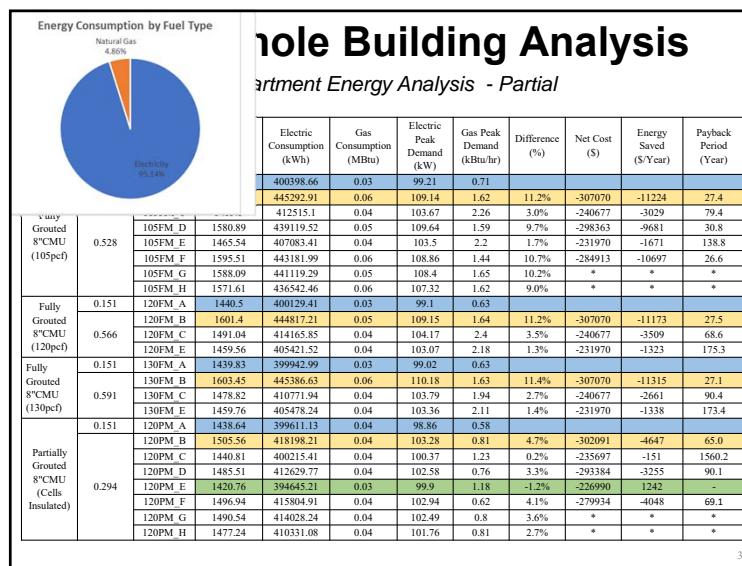
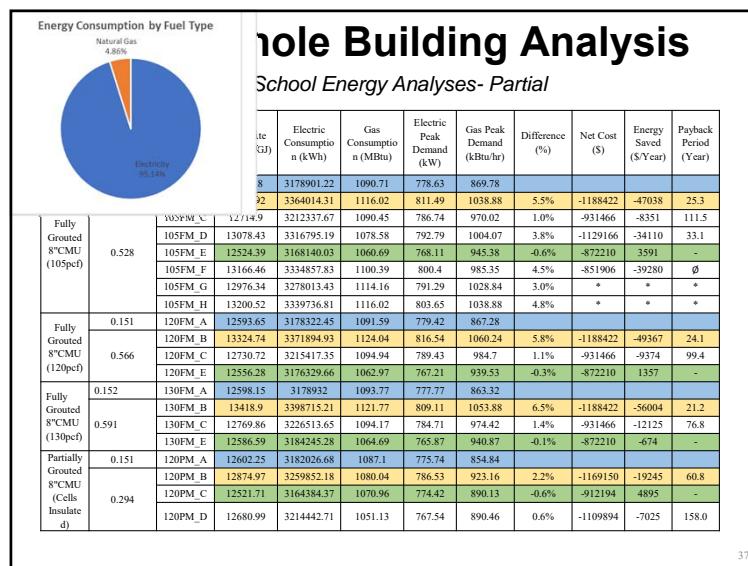


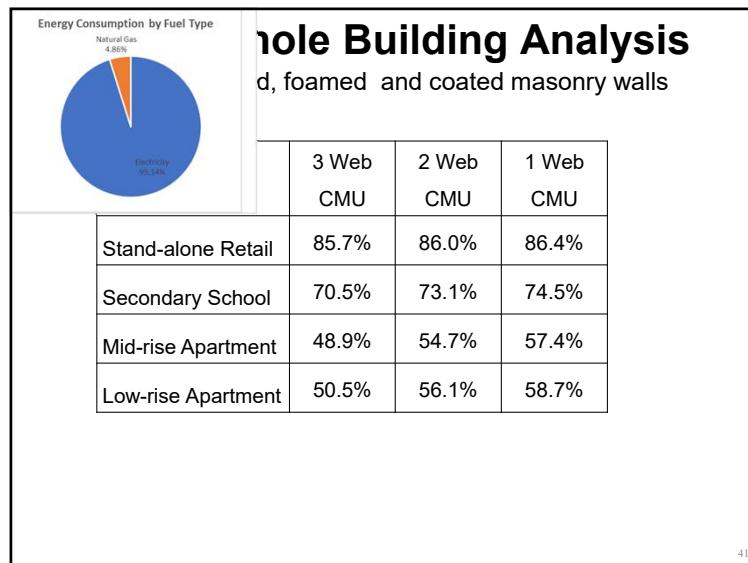
Figure 24 a) Stand-alone Retail Energy Use Break Down b) Stand-alone Retail Energy Use by Fuel





Energy Consumption by Fuel Type		Hole Building Analysis									
		Retail Energy Analyses - Partial									
Category	Sub-Category	Site ID	Electric Consumption (kWh)	Gas Consumption (MMBtu)	Electric Peak Demand (kW)	Gas Peak Demand (kWh/yr)	Change (%)	Net Cost (\$)	Energy Saved (\$/Year)	Payback Period (Year)	
		123	332747.26	58.14	84.51	100.23					
Fully GROUTED 8"CMU (105pcf)	0.528	3.69	362581.83	58.19	92.71	105.17	8.5%	-234383	-7460	31.4	
		1.89	333554.37	57.9	86.78	111.27	2.0%	-183705	-195	944.1	
		105FM_D	1360.36	360828.51	58.18	93.16	105.15	8.0%	-232003	-7022	33.0
		105FM_E	1255.9	331889.7	57.97	87.26	103.75	-0.3%	-181325	219	-
		105FM_F	1341.91	357700.73	58.18	90.3	107.19	6.6%	-169523	-5740	Ø
	0.151	105FM_G	1316.84	348747.42	58.15	89.15	104.67	4.6%	*	*	*
		105FM_H	1337.91	354587.06	58.19	89.68	105.17	6.2%	*	*	*
		120FM_A	1260.17	333008.73	58.13	84.49	100.38				
		120FM_B	1373.34	364430.67	58.19	92.98	106.08	9.0%	-234383	-7857	29.8
		120FM_C	1262.87	333813.64	57.95	86.81	100.54	0.2%	-183705	-196	938.1
Partially GROUTED 8" CMU (Cells Insulated)	0.566	120FM_E	1257.26	332258.95	57.94	87.3	100.53	-0.2%	-181325	193	-
		0.151	120PM_A	1261.75	333421.53	58.22	84.24	101.32			
		120PM_B	1294.54	342517.31	58.27	87.23	104.07	2.6%	-230576	-2275	101.3
		120PM_C	1246.22	329184.87	57.96	84.44	100.1	-1.2%	-179886	1067	-
		120PM_D	1288.99	340972.56	58.28	87.75	103.85	2.2%	-228196	-1890	120.8
	0.294	120PM_E	1243.52	328483.51	57.97	85.04	100.09	-1.4%	-177518	1255	-
		120PM_F	1288.7	340852.76	58.41	85.43	104.3	2.1%	-165716	-1864	Ø
		120PM_G	1242.29	328010.81	58.25	83.59	103.51	-1.5%	*	*	*
		120PM_H	1268.62	335318.95	58.27	84.5	104.07	0.5%	*	*	*



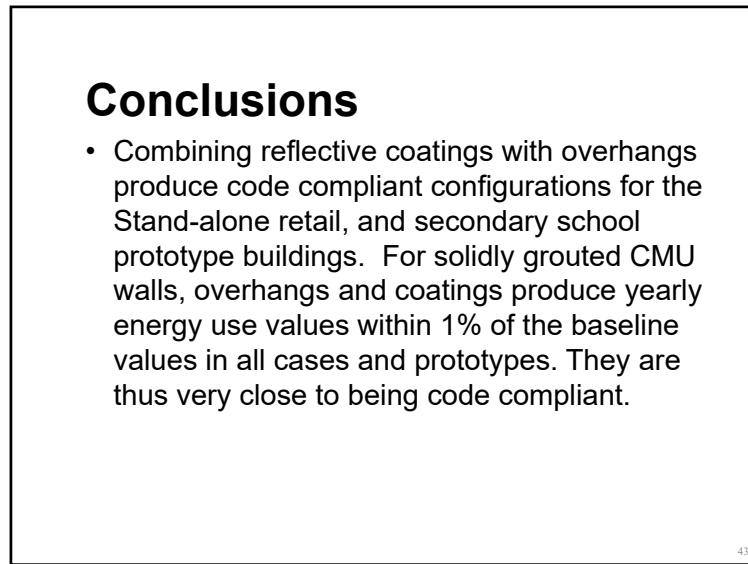


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Conclusions

- For all four prototypes (Stand-alone retail, secondary schools, mid-rise apartments and low-rise apartments), adding reflective coating is an efficient method for reducing the energy use in Hawaii's climate. In a number of exterior wall configurations, this reflective coating alone is sufficient to produce equivalent energy performance.

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Conclusions

- Reflective coatings and window shades (overhangs) have the greatest impact on energy use in the range of building types investigated. In every case addressed, the coatings and overhangs were able to reduce the yearly energy consumption values either below the baseline configuration (and code compliant), or to low enough levels of energy consumption that the difference between the baseline energy yearly costs would take well beyond the typical building design life to payback

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THANK YOU !

QUESTIONS?